FUEL OIL ASH CORROSION RESISTANCE OF ALLOYS 60 Cr:40 Ni, 50 Cr:50 Ni and 10 Al:90 Fe

> Evaluation Report NETL Test R-228 NEW-013-120

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APPROVAL IMPORMATION

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ABSTRACT

Alloys 60 Cr:40 Ni, 50 Cr:50 Ni, 10 Al:90 Fe and 25 Cr:20 Ni were tested for high temperature corrosion resistance to synthetic fuel oil ash resoldues. Compared to Alloy 25 Cr:20 Ni, Alloys 60 Cr:40 Ni and 50 Cr:50 Ni had superior corrosion resistance after 100 hours at 1700 F. to both high runadium and carbon bearing high sodium sulfate corrodents. Alloy 10Al:90 Fe had inferior corrosion resistance to both corrodent media. Resistance to scaling of 60 Cr:40 Ni alloy after 685 hours of prolonged air oxidation at 2000 F. was superior to 50 Cr:50 Ni and 25 Cr:20 Ni alloys.

SUMMARY PAGE

The Problem

To determine the relative high temperature corrosion resistance and conling characteristics of alloys 25 Cr:20 Ni, 60 Cr:40 Ni, 50 Cr:50 Ni and 10 Al:50 Fe.

lir.dings

- a. Alloy 60 Cr:40 Ni had superior high temperature corrosion resistance to synthetic fuel oil ash residues and also superior resistance to high temperature scaling.
- b. Alloy 50 Cr:50 Ni had good overall corrosion and oxidation resistance.
- c. Alloy 25 Cr:20 Ni had inferior corrosion and air oxidation resistance.
 - d. Alloy 10 Al:90 Fe had inferior corresion resistance.

<u>Foccurrendations</u>

Service tests be conducted with "dog bone" superheater support sections fabricated from 60 Cr:40 Ni and 50 Cr:50 Ni alloys.

ADMINISTRATIVE INFORMATION

Costs were charged to Project Order 60007/56. The index number is NSM-013-420.

This report covers part of an investigation of the high temperature corresion resistance of materials and alloys to synthetic fuel oil ash residues.

NOT REPRODUCIBLE

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REPORT OF INVESTIGATION

Introduction

The Naval Boiler and Turbine Laboratory is conducting a research and conformint program to obtain metals or materials with superior high temperature corresion resistance to synthetic fuel oil ash residues. This conduction test represents a phase of this program.

Tescrapiton of Materials

Test materials were:

a. Alloy 50 Cr:50 Ni

Initial specimen was a $2^n \times 2^n \times 2^{-1/2^n}$ porous section of an ingot east for experimental test purposes.

- b. Alloy 10 Al:90 Fe
 Initial specimen was 8" x 1=1/8" x 1/8" section of plate.
- Test specimens were cut from east "dog bone" sections furnished for test.
 - d. Alloy 25 Cr:20 Ni

c. Alloy 60 Cr:40 Ni

Control specimens of this material were machined from 1/8" wrought

In order to obtain sound specimens from the spongy, porous section of 10 0:150 Ni alloy, specimen dimensions were reduced to 1/8" x 5/32" x 7/8". Calar alloys tested were also machined to these dimensions. All test 1 0:001016 except the 25 Cr:20 Ni alloy were furnished the Laboratory by the 1 0:00111424.

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Modhed of Tost

a. Comrecter Postebance Tests

A set of test specimens of each alloy was weighted, partially immerced in correlent mixtures contained in porcelain crucibles, and hooked at 1700 F. in an electric furnace for increasing lengths of the up to 100 hours. Specimens were removed from the furnace at predetermined time intervals, descaled by combined mechanical and chemical cleaning, again weighed and percent weight loss determined. Test conditions were:

Corrodents Used:

- (1) High Vanadium 5 G. (15% $Na_2SO_4 \circ 65\% V_2O_5$).
- (2) High Sodium Sulfate Carbon Bearing 10 G. (90% Na₂SO₄·10% V_2O_5) + 4.3 G. (erbon.

Time Increments for:

Corrections (1) = 1, 2.5, 4, 6, 22, 46, 70 and 100 hours.
Corrections (2) = 22, 46, 70 and 100 hours.

Temperature - 1700 F.

Metals Tested - 25 Cr:20 Ni, 60 Cr:40 Ni, 50 Cr:50 Ni and 10 Al:90 Fe ollows.

Substitute Dimension = $1/3^{\circ}$ x $5/32^{\circ}$ x $7/8^{\circ}$.

b. The Constition Productions Tark

The parely note that placed in percelain emplies and heater in an closteic furn so at 2000 F. for 685 hours. Samples were removed periodically, the periodically changed to a prove loose scale and reinstalled in the formation, and the control of the conditions was a

Corrodent - Air.

Time Increments for Weight Loss Determinations = 24, 96, 192, 288, 424, 536 and 686 hours.

Temperature - 2000 F.

Metals Tested - 25 Cr:20 Ni, 60 Cr:40 Ni and 50 Cr:50 Ni. Specimen Dimensions - $1/8^n \times 5/32^n \times 7/8^n$.

Discussion and Results

Test specimen that could be salvaged from the porous, epongy section of 50 Cr:50 Ni casting were of dimensions $1/8" \times 5/32" \times 7/8"$. Similarly sized specimens were machined from control alloy 25 Cr:20 Ni and test alloys 60 Cr:40 Ni and 10 Al:90 Fe. Since this specimen size was greatly different from the usual $2" \times 1" \times 1/4"$ or $4" \times 1" \times 1/8"$ specimen sizes, 100 hour corrosivity vs. time tests were conducted instead of the usual tests of 5 hours or 20 hours duration.

An iritial 100 hour test was conducted at 1700 F. using corrodents

(a) 5 G. (15% Na₂SO₄.85% V₂O₅) and (b) 5 G. (90% Na₂SO₄.10% V₂O₅) + 2.14 G.

Carbon. A suitable range of weight losses resulted for all alloys tested in high vanadium content mixture (a). However, high sodium sulfate-carbon to mixture (b) caused little corrosion to any of the alloys. Since harber of test specimens was limited, the same specimens used in carbon bearing corrodent were subjected to another 100 hour test and corrodent weight was doubled to 10 G. (90% Na₂SO₄.10% V₂O₅) + 4.28 G. Carbon. This had sufficient corrosion resulted to afford comparison of the four alloys.

While appears to be a constant quality of reactable required to cause the character corrector for system (90% $10250_4 \cdot 103 \cdot 920_5$) + Carbon, the reacon

for this phenomenon being unknown. Corrosion vs. time curves at 1700 F. are shown for the various alloys in high vanadium corrodent, Plate 3 and high sodium sulfate carbon bearing corrodent, Plate 4. Test data is listed in Table I below:

TABLE I

Corredent - 5 G. (15% Na₂SO₄ · 85% V₂O₅), Temperature - 1700 F.

Specimen Weight Loss - Percent

Time - Hours								
Alloy	1.0	2.5	4.0	6.0	22	<u>16</u>	_70_	_100_
25 Cr:20 Ni	45.4	67.2	81.3	90.5	100	100	100	100
11 11 11 11		ent in	79.2	87.4	100	100	100	100
60 Cr:40 Ni	7.9	9.5	12.4	17.3	33.2	59.2	71.5	87.1
50 Cr:50 Ni	7.2	9.9	13.7	17.1	35.4	60.4	94.3	100
10 Al:90 Fe	€⁄->	⇔ ≈	e T	-	100	100	100	1.00

Corrodent - 10 G. (90% $Na_2SO_4 \circ 10\% V_2O_5$) + 4.3 G. Carbon, Temperature - 1700 F.

Specimen Weight Loss - Percent

		Time - Hours		
Alex	_5_	10	46	100
25 Cr:20 Ni	100	100	100	100
n ii n e	100	100	100	100
60 Cr:40 Ni	1.4	2.2	3.7	7.4
50 Cr:50 Ni	2.4	3.8	6.2	10,4
10 Al:90 Fe	55.0	63.1	701	72.5

Alloys 60 Cr:40 Ni and 50 Cr:50 Ni resist high vanadium attack much bester than do alloys 25 Cr:20 Ni and 10 Al:90 Fe. Alloy 60 Cr:40 Ni is

somewhat more resistant than 50 Cr:50 Ni. However, both alloys are severely attacked as time increases and corrosion vs. time relationship is approximately linear. The test specimens after descaling are shown in Plate 1.

Corrosion resistance of 60 Cr:40 Ni and 50 Cr:50 Ni alloys to attack caused by the high sodium sulfate carbon bearing corrodent is excellent.

Alloys 25 Cr:20 Ni and 10 Al:90 Fe suffer catastrophic attack in short periods of time in this type corrodent. Specimens of 25 Cr:20 Ni alloy were completely consumed during the first five hours of test. Plateau of curve for 10 Al:90 Fe alloy after approximately ten hours is typical for carbon bearing corrodents and represents time at which corrosive sodium sulfide is depleted. Alloy 60 Cr:40 Ni again appears slightly more resistant than 50 Cr:50 Ni. The test specimens after descaling are shown in Plate 2.

Alloys 60 Cr:40 Ni and 50 Cr:50 Ni evidenced corrosion patterns similar to those of 25 Cr:20 Ni alloy in both types of corrodent. In high vanadium corrodent metal surfaces were substantially smooth and uniform as though metals were being dissolved. However, in high sodium sulfate carbon bearing mixture, corrosive attack was more localized with heavy pitting in some cases. The 10 Al:90 Fe alloy was consumed by high vanadium corrodent and suffered severe penetration and embrittlement in high sodium sulfate carbon bearing mixture in relatively short periods of time.

A prolonged air oxidation test was conducted at 2000 F. to compare relative high temperature scaling resistance of alloys 25 Cr:20 Ni, (10.0.:40 Ni and 50 Cr:50 Ni. Test was run for 685 hours. Curves of percent with loss was time in Plate 5 show 60 Cr:40 Ni to have best resistance to high temperature scaling with 50 Cr:50 Ni next best and 25 Cr:20 Ni alloy terms. Test data is listed below, Table II.

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TABLE II

Corrodent - Air; Temperature - 2000 F.

Specimen Weight Loss - Percent

Time - Hours

Mor	24	96	192	288	1.24	<u>536</u>	685
25 Cr:20 Ni	0,2	0.9	2.0	2.3	4.1	12.6	14.1
60 Cr:40 Ni	0.4	1.0	1.3	1.4	1.7	2.1	2.4
50 Cr:50 M	0.7	2,1	3.7	4.3	5.4	6.3	6.7

It is of interest to note that 25 Cr:20 Ni alloy shows less scaling up to 424 hours than does 50 Cr:50 Ni alloy, then in the next time increment shows excessive scaling after which curve again assumes its previous slope. Visual observations of the test specimen substantiated the experimental data cines it was noticed that at 460 hour time increment a thick oxide coating apalled from the 25 Gr:20 NL specimen.

Conclusions

- a. Alloys 60 Cr:40 Ni and 50 Cr:50 Ni are superior to 25 Cr:20 Ni alloy in high temperature corrosion resistance to synthetic fuel oil ash residues. Here are entremely resistant to sulfide attack caused by carbon bearing corrodents of high sodium sulfate content. They are considerably more resistant to corrodents of high vanadium content than is 25 Cr:20 Ni alloy.
- b. Alloy 60 Cr:40 Hi is considered to have somewhat better corresion will beach than alloy 50 Cr:50 Ni.
- C. Those alloys also have better resistance to high temperature scalusive blue does 25 Gra20 Mi alloy. Alloy 60 Gra40 Mi is more resistant than alloy 50 Gra50 Mi.
 - d. Alloy 10 Al:90 Fe has inferior high temperature corrosion

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- 1, It is recommended that:
- a. "Dog bone" type superheater support elements be fabricated from Or:40 Mi alloys and that these parts be service tested.
- b. Allow 10 Al:50 Fe be considered unsuitable for naval use in highly corrosive environments at elevated temperatures.

CRUCIBLE TESTS NBTL TEST R-228 SPECIMENS AFTER DESCALING

TEMP 1700*F

CORROCERT 5 6 1512 50, 85V_OF

INITIAL SPECIMEN SIZE 7/8"X 5/32"X 1/8"

TIME	25 Cr. 20 Ni	60CR : 40 NI	50 CR : 50NI
нкs. I			G.NOW
2.5		<u> </u>	Carr
4	Circin		E 543
6	******	<u>& 703</u>	E
22		CHES	
46		•	
70		· ·	

PLATE !

SOAL: BOFE CORRODENT 10G (90% Ng 2504 10% V205) + 4.3 G CARBON Die a . 50 CR: 50NI THE PARTY OF THE P 322 INITIAL SPECIMEN SIZE 7/8"X 5/32"X 1/8" 60 CR : 40 NI SPECIMENS AFTER DESCALING CRUCIBLE TESTS TEMP. 1700*F 25 Cr 20Ni TIME HRS. 8 4 0

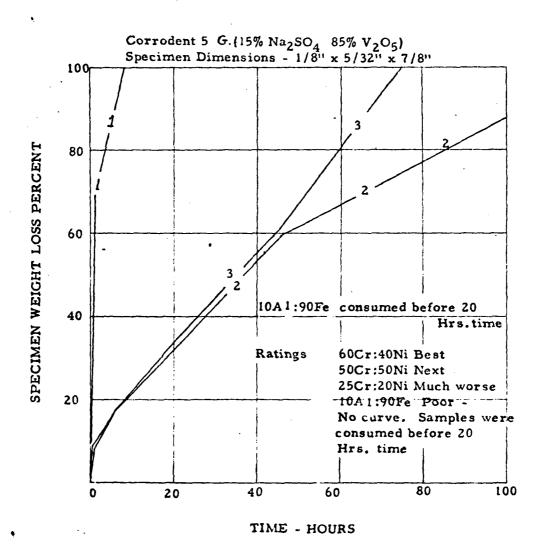
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PLATE 2

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Crucible Corrosion Tests of Alloys 25Cr:20Ni, 60 Cr:40Ni, 50Cr:50Ni and 10Al:90Fe in High Vanadium-Corrodent

LEGEND
1-1 25Cr:20Ni
2-2 60Cr:40Ni
3-3 50Cr:50Ni



Crucible Corrosion Tests of Alloys 25Cr:20 Ni, 60Cr: 40Ni, 50Cr:50Ni and 10 Al:90Fc in High Sodium Sulfate Carbon Bearing Corrodent

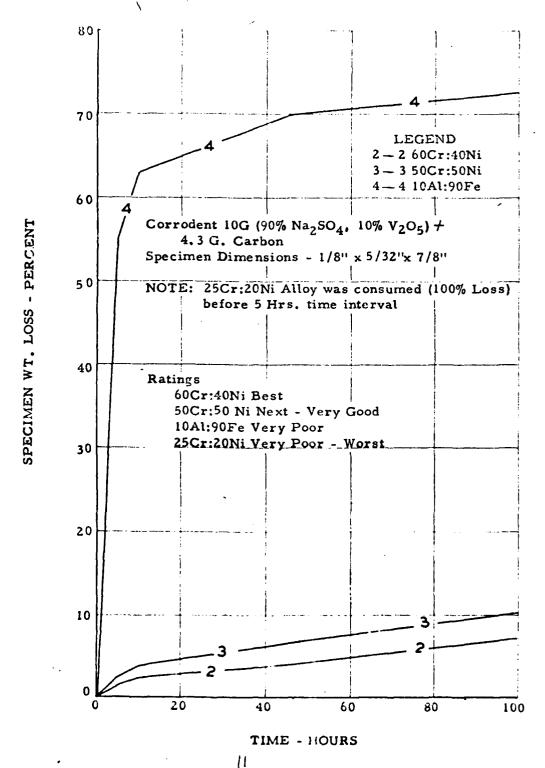
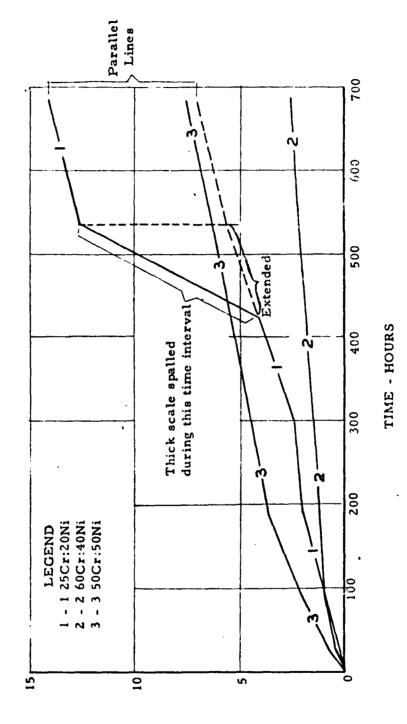


PLATE 4

AIR OXIDATION OF REFRACTORY ALLOYS AT 2000 F



WEIGHT LOSS (SCALING) - PERCENT